

The Modal-Vertical-Beam(MVB) Transmission Loss Analysis

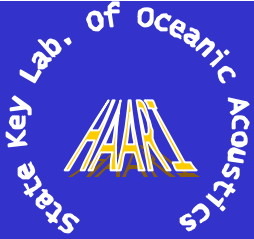
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Main Scientific Objective

- **Extraction the beam-averaged modal attenuation coefficient d_n**

How to do?

Step 1: Perform vertical plane wave beamforming with VLA acoustic data

Step2: Estimate the beamformer output spectrum

Step3: Calculate propagation loss of two different ranges

Step4: Extract the beam-averaged modal attenuation coefficient from propagation loss

Why to do?

Be important for bottom back-scattering matrix extraction from reverberation data as well as propagation modeling

Theory Frame

The complex pressure in a range-independent waveguide can be written as:

$$p(r, z_j, z_s, \mathbf{w}) = \sum_{n=0}^{N-1} a_n(r) \mathbf{j}_n(z_j) \mathbf{j}_n(z_s) \exp[-i(\mathbf{w}t - k_n r + \mathbf{p} / 4) - \mathbf{d}_n r]$$

For an ideal spatial filter response, the beamformer output can be written as:

$$b(r, \bar{\gamma}, z_s, \omega) = \sum_{\bar{m}-\Delta m/2}^{\bar{m}+\Delta m/2} a_n(r) \varphi_n(z_s) \exp[-i(\omega t - k_n r + \pi / 4) - \delta_n r]$$

The vertical beamformer output spectrum is

$$\begin{aligned} B(r, \gamma_n, z_s, \omega) &= \sum_n a_n^2(r) \varphi_n^2(z_s) \exp(-2\delta_n r) \\ &\quad + 2 \sum_n \sum_{\substack{m \\ n \neq m}} a_n(r) a_m(r) \varphi_n(z_s) \varphi_m(z_s) \exp(-(\delta_n + \delta_m)r) \cos(\Delta k_{nm} r) \\ &= B_1 + B_2 \end{aligned}$$

Theory Frame(continued)

If $B_2 \ll B_1$, the beamformer output spectrum is written as:

$$B(r, \gamma_n, z_s, \omega) = \sum_n a_n^2(r) \phi_n^2(z_s) \exp(-2\delta_n r)$$

We define the beam-averaged modal attenuation as follow:

$$\exp(-2\delta_{\bar{m}} r) = \frac{\sum_{\bar{m}-\Delta m/2}^{\bar{m}+\Delta m/2} a_n^2(r) \phi_n^2(z_s) \exp(-2\delta_n r)}{\sum_{\bar{m}-\Delta m/2}^{\bar{m}+\Delta m/2} a_n^2(r) \phi_n^2(z_s)}$$

Beam-averaged modal attenuation coefficient can be extracted by calculating the propagation loss for two ranges:

$$\delta_n = \frac{\log(\text{tl}(r_1, r_2))}{2(r_2 - r_1)} \quad \text{Where,} \quad \text{tl}(r_1, r_2) = \frac{B(r_1, \gamma_n, z_s, \omega) \times r_1}{B(r_2, \gamma_n, z_s, \omega) \times r_2}$$

Numerical Simulation

We consider a Pekeris waveguide : $H=103\text{m}$, $C_0=1519\text{m/s}$, $C_b=1623\text{m/s}$, $\gamma_b=1.72$, $\alpha_b=0.49\text{ dB/m}\cdot\text{kHz}$, $f=1390\text{Hz}$. The 103m VLA is covered all depth of water column with 1m space of adjacent element.

Table 1 Theoretical value and calculated value of δ_n in Pekeris waveguide ($f=1390\text{Hz}$)

group	Center grazing angle	Group of modes	Theory value of δ_n	Calculated value of δ_n	
				$r1=10\text{km}, r2=20\text{km}, z_s=20\text{m}$	$r1=10\text{km}, r2=20\text{km}, z_s=40\text{m}$
1	$2.3_i \tilde{\alpha}$	1-8	$3.367554\text{e-}6$	$-5.030152\text{e-}6$	$3.158571\text{e-}6$
2	$6.8_i \tilde{\alpha}$	9-16	$2.051041\text{e-}5$	$3.249568\text{e-}5$	$1.507090\text{e-}5$
3	$11.5_i \tilde{\alpha}$	17-24	$5.064872\text{e-}5$	$3.641855\text{e-}5$	$5.898481\text{e-}5$
4	$16.2_i \tilde{\alpha}$	25-32	$9.020034\text{e-}5$	$9.085626\text{e-}5$	$8.014695\text{e-}5$

Due to the effect of intermode interference , δ_n of group 1 can not be estimated correctly, and the precisions of estimated δ_n of other groups are poor.

Numerical Simulation(continued)

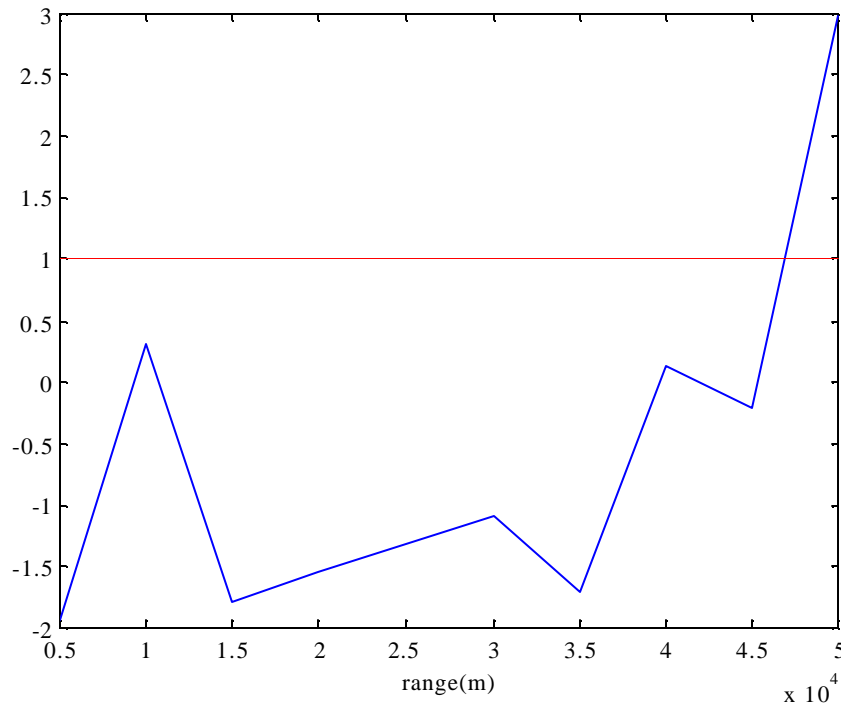
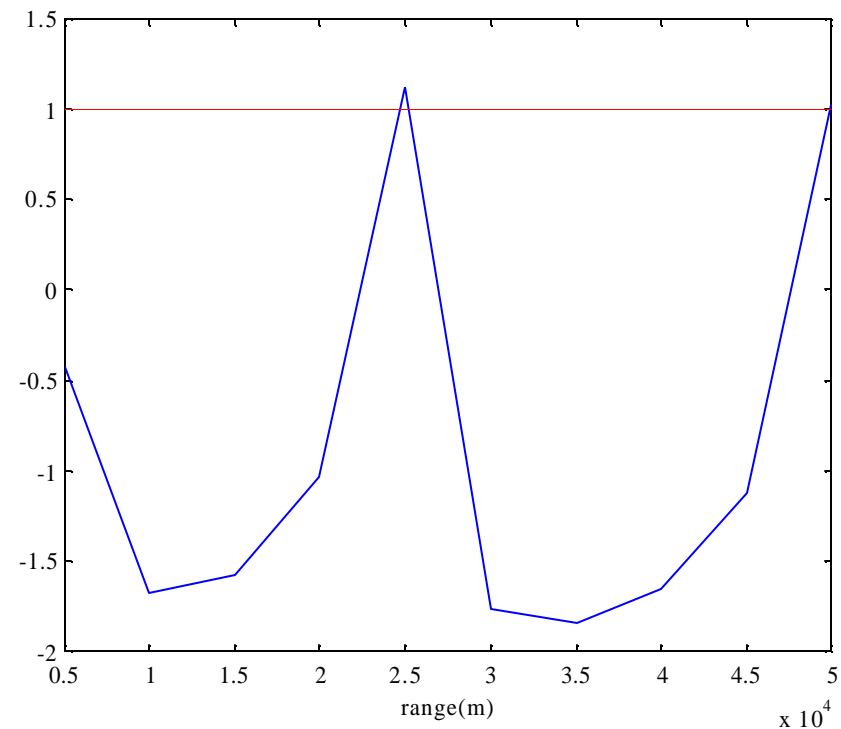


Fig.1 Effect of intermode interference
($f=1390\text{Hz}$, $z_s=20\text{m}$)

Fig.2 Effect of intermode interference
($f=1390\text{Hz}$, $z_s=40\text{m}$)

Effects of intermode interference
can not be ignored



Numerical Simulation(continued)

How can we reduce the effects of intermode interference? One method is averaged the beamformer output spectrum with f in a narrow band to smooth second item B_2 .

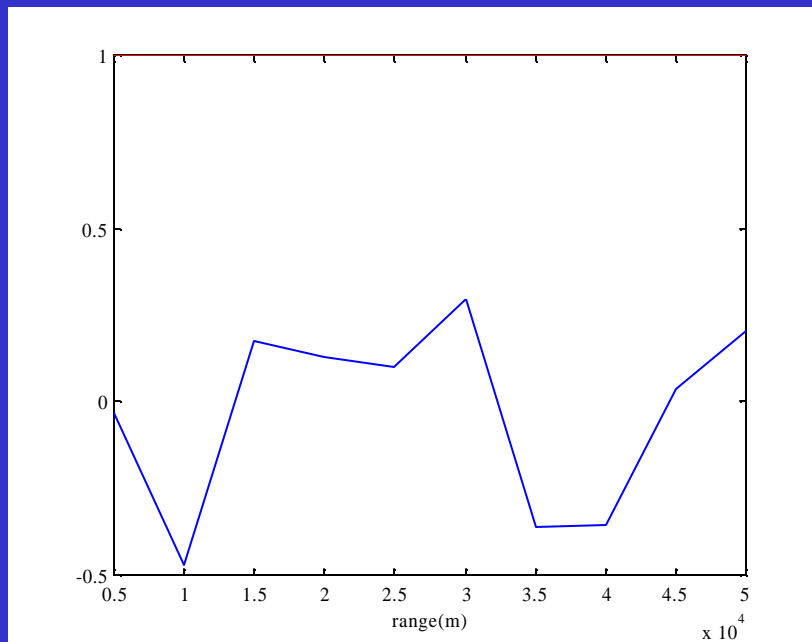


Fig.3 Effect of intermode interference ($f=1340-1440\text{Hz}$, $z_s=20\text{m}$)

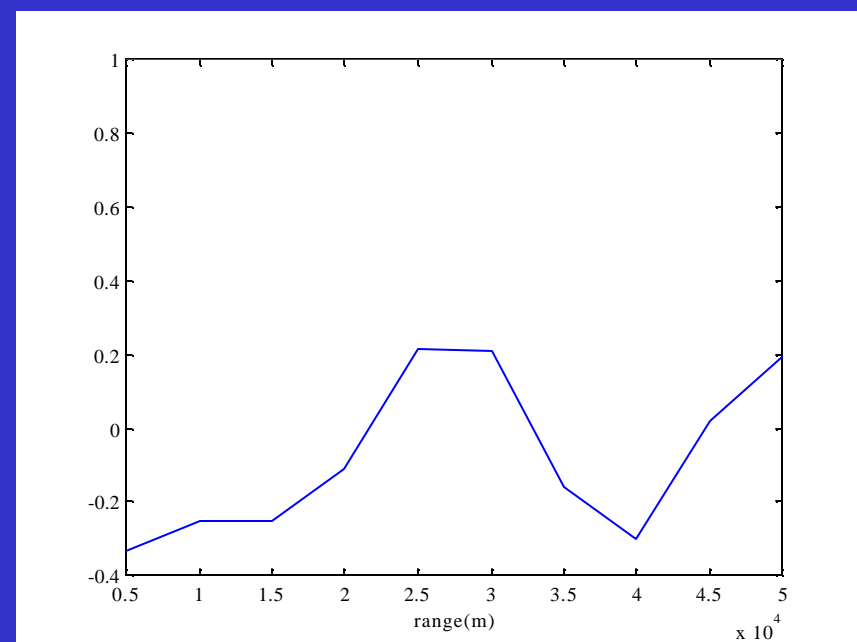


Fig.4 Effect of intermode interference ($f=1340-1440\text{Hz}$, $z_s=40\text{m}$)

Numerical Simulation(continued)



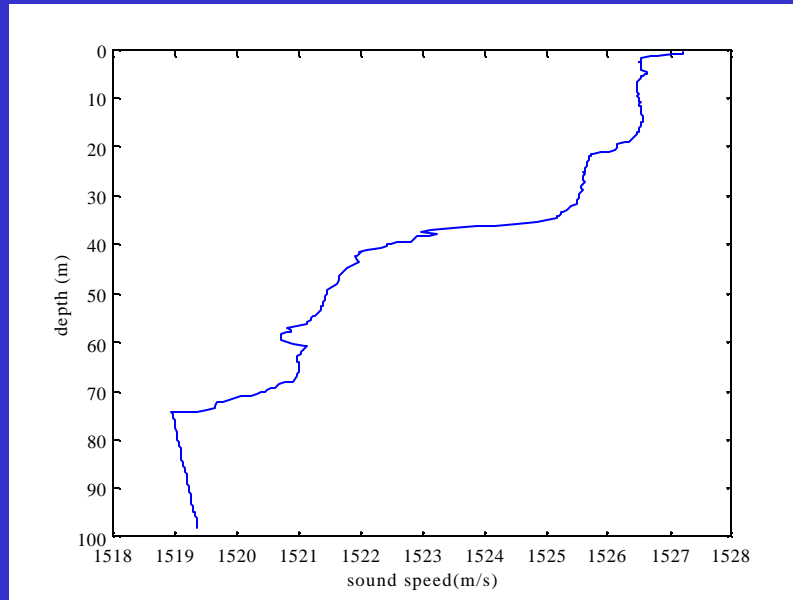
Table 2 Theory value and calculated value of δ_n in Pekeris waveguide (f=1340-1440Hz)

group	Center grazing angle	Group of modes	Theory value of δ_n	Calculated value of δ_n		
				r1=5km, r2=10km, zs=40m	r1=10km, r2=20km, zs=40m	r1=10km, r2=20km, zs=20m
1	2.3 _j \tilde{a}	1-8	3.143104e-6	7.894265e-6	1.705594e-6	3.646730e-6
2	6.8 _j \tilde{a}	9-16	1.918959e-5	1.920825e-5	2.095787e-5	1.802004e-5
3	11.5 _j \tilde{a}	17-24	4.754961e-5	4.799638e-5	4.731562e-5	4.815836e-5
4	16.2 _j \tilde{a}	25-32	8.491166e-5	8.500221e-5	8.566655e-5	8.432893e-5

Compared to Table 1, the attenuation coefficients of all groups can be estimated, the precision is also improved effectively.

Numerical Simulation(continued)

Fig. 5
SVP
of
ECS



All the calculated d_n are larger than the theoretical values. This is due to:

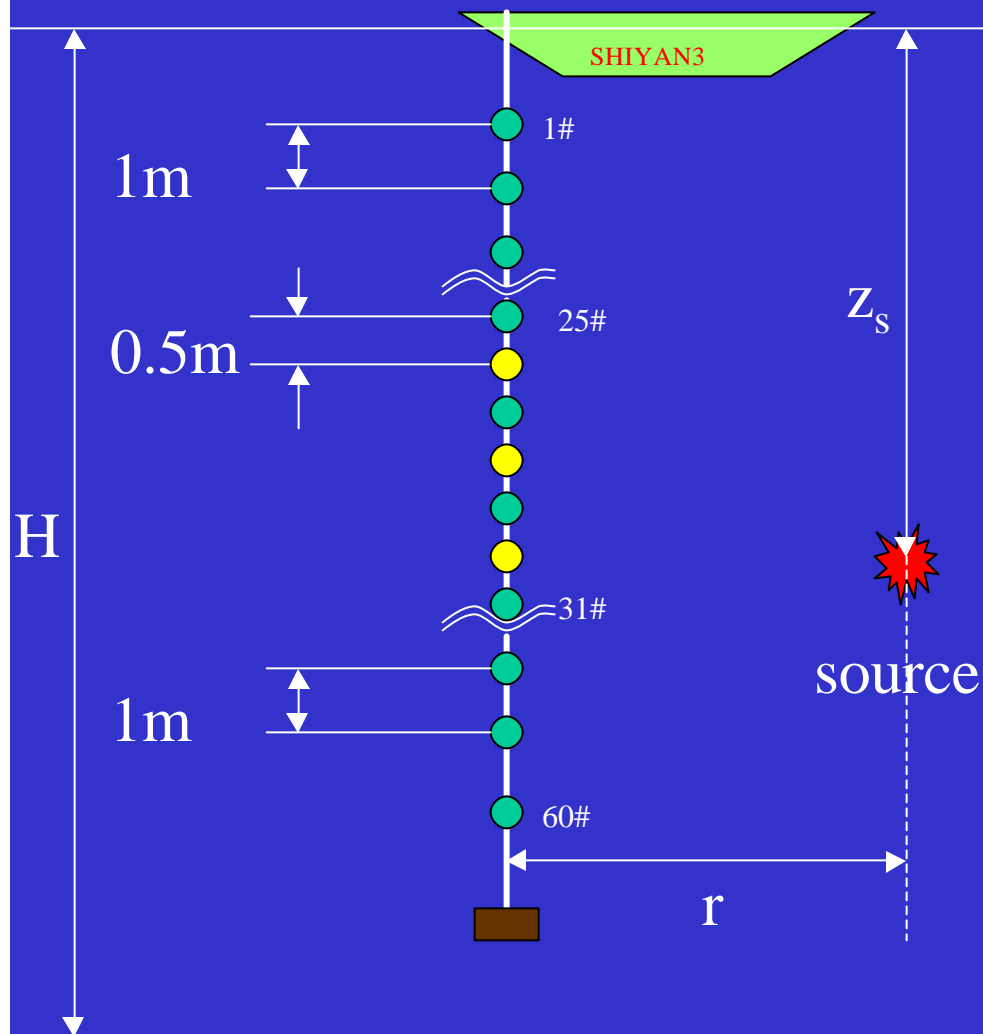
- (1) effect of inter mode interference
- (2) the short VLA covered the upper half part of the water column is not able to capture the lower modes properly and affected by higher modes by leakage.

Table 3 Theoretical value and calculated value of δ_n in simulated shallow waveguide (f=1340-1440Hz)

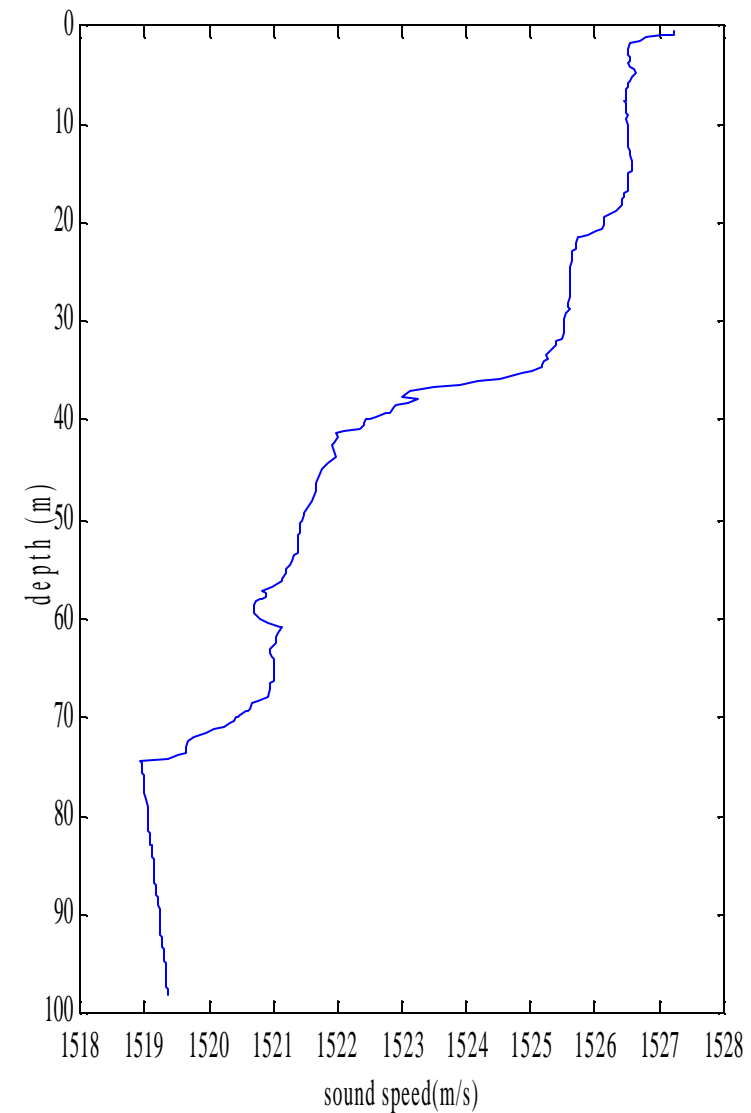
group	Center grazing angle	Group of modes	Theory value of δ_n	Calculated value of δ_n	
				r1=10km,r2=20km, zs=40m, 103mVLA	r1=10km,r2=20km, zs=40m,57mVLA
1	2.3; \tilde{a}	1-8	6.011310e-6	2.193981e-5	1.630264e-5
2	6.8; \tilde{a}	9-16	2.272945e-5	3.075102e-5	4.356382e-5
3	11.5; \tilde{a}	17-24	3.601585e-5	5.283101e-5	6.074829e-5
4	16.2; \tilde{a}	25-32	8.115852e-5	8.317109e-5	1.071509e-4

ECS Real data analysis

Experiment setup



● Not used in this paper



ECS Real data analysis (continued)

Experiment setup

- Receiving array: 60-element VLA, from 3m to 60m
- Source: locating at different depths $z_s=5\text{m}$, 20m, 40m, and different ranges $r=5\text{km}$, 10km, 20km and 30~40km
- Water depth: $H=103\text{m}$
- Signal forms: 1100-2000Hz PRN, 630Hz CW, 630Hz PCW, 1250-2500HZ LFM, and explosive sources

In our talk, only signals of 1100-2000Hz PRN at ranges of 5km and 10km, depths of 20m and 40m are used to estimated beam-averaged δ_n now.

ECS Real data analysis (continued)

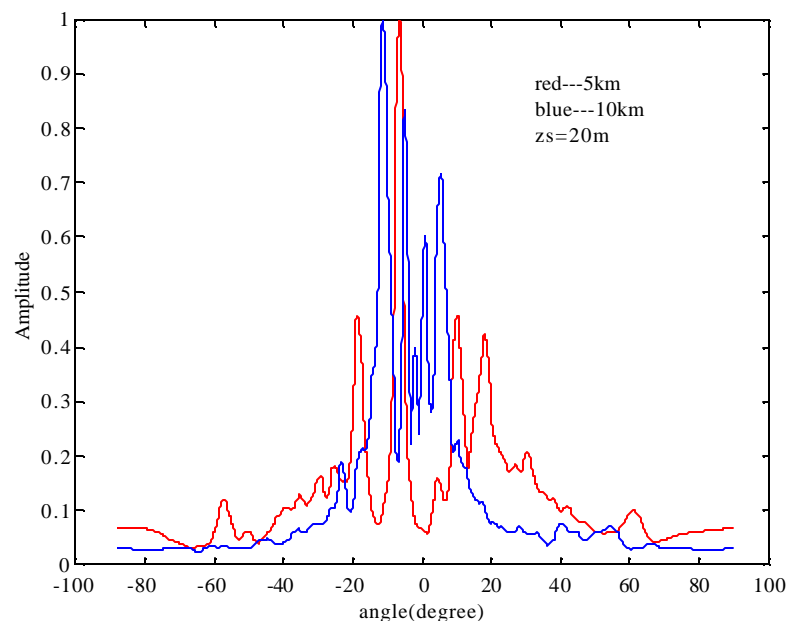


Fig.6 Vertical beam pattern with 20m source depth

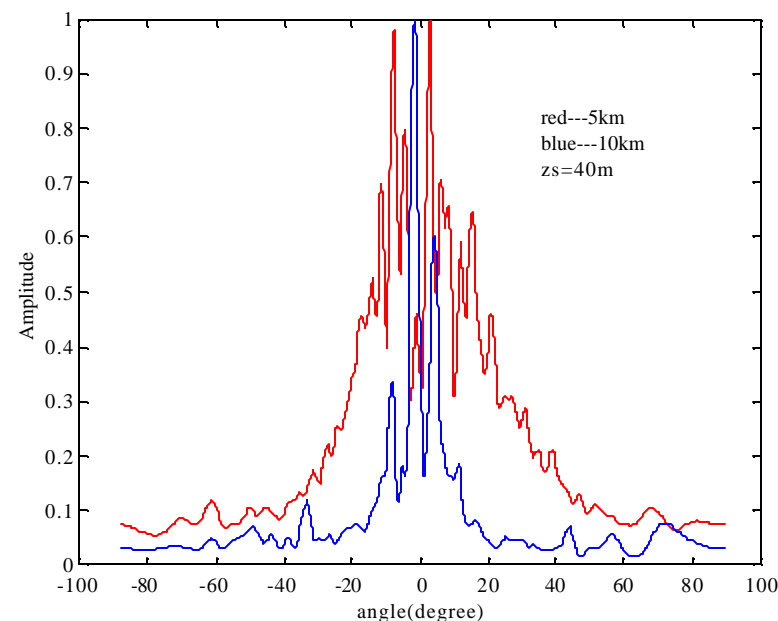


Fig.7 Vertical beam pattern with 40m source depth

Table 4 The estimated value of δ_n in real shallow waveguide (f=1340-1440Hz)

group	Center grazing angle	Group of modes	Estimated value of δ_n	
			r1=5km,r2=10km, zs=20m	r1=5km,r2=10km, zs=40m
1	2.3 _i ã	1-8	1.195583e-4	2.785835e-5
2	6.8 _i ã	9-16	2.447215e-4	1.224623e-4
3	11.5 _i ã	17-24	1.853596e-4	1.175435e-4
4	16.2 _i ã	25-32	2.953209e-4	1.934406e-4

Summary

- If the intermode sum can be ignored, the beamformer output spectrum of two different ranges can be used to extract beam-averaged modal attenuation coefficient.
- When vertical beamformer is performed in a narrow band not in single tone, the intermode sum can be reduced effectively, as proved by the numerical examples, but it is still large, should be decreased further.
- From numerical simulation and ECS real data analysis results, we should extract beam-averaged modal attenuation coefficient from data collected by longer VLA covered all water column in a broader band.



Thank you!